#F## 17517FD 09 FEB 2006

······ to obtain a honeycomb formed material having a partition wall (partition wall 2 in Fig. 2) thickness of 310 μm, a cell density of 46.5 cells /cm² (300 cells/in.², a square section of 35 mm x 35 mm and a length of 152 mm. The formed material was subjected to debinding at 400°C in the atmosphere and then fired at about 1,450°C in an Ar inert atmosphere to obtain a porous honeycomb structure (honeycomb segment) made of SiC bonded with Si.

[0059]

The honeycomb segment was measured for average pore diameter by mercury porosity, as wall as for porosity by the Archimedes method. As a result, the honeycomb segment was a carrier having a porosity of 52% and an average pore diameter of 20 μ m. This honeycomb segment is termed "base material A".

15 [0060]

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A SiC powder having an average particle diameter of 12 µm as a ceramic raw material, iron oxide and yttrium oxide each as a sintering aid, methyl cellulose as an organic binder, starch as a pore former, a surfactant and water were kneaded by a vacuum pug mill to produce a plastic puddle.
[0061]

The puddle was subjected to extrusion to obtain a honeycomb structure. The honeycomb structure was dried using a microwave and hot air to obtain a honeycomb formed material having a partition wall thickness of 310 μ m, a cell density of 46.5 cells /cm² (300 cells/in.²), a square section of 35 mm x 35 mm and a length of 152 mm. The formed material was subjected to debinding at 550°C in the atmosphere and then fired at 2,300°C in an Ar inert atmosphere to obtain a porous honeycomb structure (honeycomb segment) made of

recrystallized SiC.

[0062]

The honeycomb segment was measured for average pore diameter by mercury porosity, as wall as for porosity by the Archimedes method. As a result, the honeycomb segment was a carrier having a porosity of 42% and an average pore diameter of 10 μ m. This honeycomb segment is termed "base material B". [0063]

Next, the base materials A and B produced above were subjected to a heat treatment by a method shown in Table 1, to form a film (an oxide film) on the surface.

[0064]

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In Examples 1 to 6, 13, 14, 18 and 19, the heat treatment was conducted, as shown in the following (1) and (2), by either of a method of conducting a heat treatment after firing (expressed as "After firing" in the column of "Heat treatment step" of Table 1) and a method of conducting a heat treatment after debinding but before firing (expressed as "After debinding" in the column of "Heat treatment step" of Table 1).

[0065]

(1) A method of conducting a heat treatment after firing:

A method in which, after debinding, firing is conducted in an Ar atmosphere and then a heat treatment is conducted (Examples 1 to 6, 18 and 19).

[0066]

(2) A method of conducting a heat treatment after debinding but before firing:

A method in which, after debinding, a heat treatment is conducted, and then firing is conducted in an Ar atmosphere

(Examples 13 and 14).

[0067]

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In Example 15, the heat treatment was conducted by subjecting air to bubbling using a wetter and sending an air containing water vapor (steam) into a furnace for heat treatment [expressed as "Steam blowing" in the column of "Heat treatment conditions (temp. and time)" of Table 1]. The heater temperature of the wetter was 40°C.

[0068]

10 In Examples 16 and 17, the heat treatment was conducted by burner combustion and heating using LNG (liquefied natural gas) as a fuel (expressed as "Burner combustion" in the column of "Heat treatment conditions (temp. and time)" of Table 1]. The air and fuel ratio was about 1.2 in the 15 highest temperature range.

[0069]

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In Examples 7 to 9, the heat treatment was conducted after pre-coating of sol (expressed as "ZrO2" or "Al2O3" in the column of "Pre-coating" of Table 1). That is, in Examples 7 to 8, the base material A was dipped in an alumina sol (nitric acid solution) or a zirconia sol (nitric acid solution) (as necessary, further in a silica sol) for wash coating. The amount of coating was 30 g/liter. Then, baking was conducted at a temperature shown in Table 1. After this baking, a heat treatment was conducted at a temperature shown in Table 1. After the firing, the crystalline phase formed was identified by X-ray diffraction, which confirmed formation of zircon in Examples 7 and 8 and formation of mullite in Example 9. That is, in Examples 7 to 9, the 30 treatment was conducted according to the following procedure.

Debinding was conducted; then, firing was conducted in an Ar atmosphere; thereafter, a sol was pre-coated; and a heat treatment was conducted.

[0070]

In Examples 10 to 12, a precursor was added to the raw materials and the heat treatment was conducted (expressed as "ZrO2" or "Al2O3" in the column of "Addition to raw material(s)" of Table 1). That is, in the step of production of base material A, zirconia or alumina was added to raw 10 materials in an amount of 5% by mass; firing was conducted; then, a heat treatment was conducted at a temperature shown in Table 1. After the firing, the crystalline phase formed was identified by X-ray diffraction, which confirmed formation of zircon in Examples 10 and 11 and formation of mullite in Example 12.

[0071]

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In Comparative Example 1, only firing was conducted to the base material A and no heat treatment was conducted. In Comparative Examples 2 to 4, the heat treatment was conducted at a temperature shown in Table 1, according to the method of conducting a heat treatment after firing (Comparative Examples 2 and 3) or the method of conducting a heat treatment after debinding but before firing (Comparative Example 4). In Comparative Example 5, only firing was conducted to the base material B and no heat treatment

Claims

[1] A silicon carbide-based catalyst body comprising: a porous honeycomb structure wherein silicon carbide particles as the aggregate thereof are bonded to one another with pores held among them, and

a catalyst loaded on the surface of the porous honeycomb structure, containing alumina and ceria as main components,

characterized in that the catalyst is loaded on the surface 10 of the porous honeycomb structure via a film comprising a silicon-containing oxide and that the film contains oxygen in an amount of 2 to 10% by mass of the total elements constituting the porous honeycomb structure.

A silicon carbide-based catalyst body according to Claim 1, wherein the film contains alumina and/or zirconia as the element (elements) thereof.

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- A silicon carbide-based catalyst body according to Claim 1 or 2, characterized in that the film contains, as the crystalline phase thereof, at least one member selected from the group consisting of cristobalite, zircon and mullite.
- A silicon carbide-based catalyst body according to any of Claims 1 to 3, characterized in that the silicon carbide particles are bonded by metallic silicon as the binder thereof.
- 25 A method for preparing a silicon carbide-based catalyst body, characterized by extruding a raw material containing silicon carbide particles to obtain a honeycomb structure, firing the honeycomb structure, then subjecting the fired honeycomb structure to a heat treatment in an oxygen-
- 30 containing atmosphere to obtain a porous honeycomb structure,

and loading, on the surface of the porous honeycomb structure, a catalyst containing alumina and ceria as main components.

- [6] A method for preparing a silicon carbide-based catalyst body according to Claim 5, wherein the heat treatment is conducted in an atmosphere containing oxygen and steam.
- [7] (After amendment) A method for preparing a silicon carbide-based catalyst body according to Claim 5 or 6, wherein the heat treatment is conducted by heating a target substance directly with a heat generated by burner combustion using natural gas as a fuel.

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- [8] A method for preparing a silicon carbide-based catalyst body according to any of Claims 5 to 7, wherein the heat treatment is conducted at a temperature of 800 to 1,400°C.
- [9] A method for preparing a silicon carbide-based catalyst body, characterized by extruding a raw material containing silicon carbide particles to obtain a honeycomb structure,